

[0034] FIG. 9B is a schematic view of an epicyclic gear train having a second example geometry ratio.

[0035] FIG. 9C is a schematic view of an epicyclic gear train having a third example geometry ratio.

[0036] FIG. 10 is a nomograph depicting the interrelationship of speeds of epicyclic gear train components for a given geometry ratio.

[0037] FIG. 11A is a schematic view of an epicyclic gear train having the first geometry ratio with a carrier rotating in the opposite direction to that shown in FIG. 9A.

[0038] FIG. 11B is a schematic view of an epicyclic gear train having the second geometry ratio with a carrier rotating in the opposite direction to that shown in FIG. 9B.

[0039] FIG. 11C is a schematic view of an epicyclic gear train having the third geometry ratio with a carrier rotating in the opposite direction to that shown in FIG. 9C.

DETAILED DESCRIPTION

[0040] FIG. 1 schematically illustrates a gas turbine engine 20. The gas turbine engine 20 is disclosed herein as a two-spool turboprop that generally incorporates a fan section 22, a compressor section 24, a combustor section 26 and a turbine section 28. Alternative engines might include an augmentor section (not shown) among other systems or features. The fan section 22 drives air along a bypass flowpath B while the compressor section 24 drives air along a core flowpath C for compression and communication into the combustor section 26 then expansion through the turbine section 28. Although depicted as a turboprop gas turbine engine in the disclosed non-limiting embodiment, it should be understood that the concepts described herein are not limited to use with turboprops as the teachings may be applied to other types of turbine engines including three-spool architectures.

[0041] The engine 20 generally includes a low speed spool 30 and a high speed spool 32 mounted for rotation about an engine central longitudinal axis A relative to an engine static structure 36 via several bearing systems 38. It should be understood that various bearing systems 38 at various locations may alternatively or additionally be provided.

[0042] The low speed spool 30 generally includes an inner shaft 40 that interconnects a fan 42, a low pressure (or first) compressor section 44 and a low pressure (or first) turbine section 46. The inner shaft 40 is connected to the fan 42 through a geared architecture 48 to drive the fan 42 at a lower speed than the low speed spool 30. The high speed spool 32 includes an outer shaft 50 that interconnects a high pressure (or second) compressor section 52 and high pressure (or second) turbine section 54. A combustor 56 is arranged between the high pressure compressor 52 and the high pressure turbine 54. A mid-turbine frame 57 of the engine static structure 36 is arranged generally between the high pressure turbine 54 and the low pressure turbine 46. The mid-turbine frame 57 supports one or more bearing systems 38 in the turbine section 28. The inner shaft 40 and the outer shaft 50 are concentric and rotate via bearing systems 38 about the engine central longitudinal axis A, which is collinear with their longitudinal axes. As used herein, a “high pressure” compressor or turbine experiences a higher pressure than a corresponding “low pressure” compressor or turbine.

[0043] The core airflow C is compressed by the low pressure compressor 44 then the high pressure compressor 52, mixed and burned with fuel in the combustor 56, then expanded over the high pressure turbine 54 and low pressure turbine 46. The mid-turbine frame 57 includes airfoils 59

which are in the core airflow path. The turbines 46, 54 rotationally drive the respective low speed spool 30 and high speed spool 32 in response to the expansion.

[0044] The engine 20 in one example is a high-bypass geared aircraft engine. In a further example, the engine 20 bypass ratio is greater than about six (6), with an example embodiment being greater than ten (10), the geared architecture 48 is an epicyclic gear train, such as a star gear system or other gear system, with a gear reduction ratio of greater than about 2.3 and the low pressure turbine 46 has a pressure ratio that is greater than about 5. In one disclosed embodiment, the engine 20 bypass ratio is greater than about ten (10:1), the fan diameter is significantly larger than that of the low pressure compressor 44, and the low pressure turbine 46 has a pressure ratio that is greater than about 5:1. Low pressure turbine 46 pressure ratio is pressure measured prior to inlet of low pressure turbine 46 as related to the pressure at the outlet of the low pressure turbine 46 prior to an exhaust nozzle. It should be understood, however, that the above parameters are only exemplary of one embodiment of a geared architecture engine and that the present invention is applicable to other gas turbine engines including direct drive turboprops.

[0045] A significant amount of thrust is provided by the bypass flow B due to the high bypass ratio. The fan section 22 of the engine 20 is designed for a particular flight condition—typically cruise at about 0.8 Mach and about 35,000 feet. The flight condition of 0.8 Mach and 35,000 ft, with the engine at its best fuel consumption—also known as “bucket cruise Thrust Specific Fuel Consumption (“TSFC”)”—is the industry standard parameter of lbf of fuel being burned per hour divided by lbf of thrust the engine produces at that minimum point. “Fan pressure ratio” is the pressure ratio across the fan blade alone, without a Fan Exit Guide Vane (“FEGV”) system. The low fan pressure ratio as disclosed herein according to one non-limiting embodiment is less than about 1.45. “Low corrected fan tip speed” is the actual fan tip speed in ft/sec divided by an industry standard temperature correction of $[(T_{\text{ram deg R}}/518.7)^{0.5}]$. The “Low corrected fan tip speed” as disclosed herein according to one non-limiting embodiment is less than about 1150 ft/second.

[0046] An example geared architecture 48 for the engine 20 is shown in FIG. 2. Generally, the engine static structure 36 supports the inner and outer shafts 40, 50 for rotation about the axis A. The outer shaft 50 supports the high pressure compressor section 52 and the high pressure turbine section 54, which is arranged upstream from the mid turbine frame 59.

[0047] The inner shaft 40 is coupled to the geared architecture 48, which is an epicyclic gear train 60 configured in a differential arrangement. The gear train 60 includes planetary gears 64 supported by a carrier 62, which is connected to the inner shaft 40 that supports the low pressure turbine 46. A sun gear 66 is centrally arranged relative to and intermeshes with the planetary gears 64. A ring gear 70 circumscribes and intermeshes with the planetary gears 64. In the example, a fan shaft 72, which is connected to the fan 42, is rotationally fixed relative to the ring gear 70. The low pressure compressor 44 is supported by a low pressure compressor rotor 68, which is connected to the sun gear 66 in the example.

[0048] The carrier 62 is rotationally driven by the low pressure turbine 46 through the inner shaft 40. The planetary gears 64 provide the differential input to the fan shaft 72 and low pressure compressor rotor 68 based upon the geometry ratio, which is discussed in detail in connection with FIGS. 9A-10.